

### Mock-ups of the SPL cavity supporting system

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- 1. Overview of cavity supporting system
- 2. Double tube mock-up
- 3. Supporting system mock-up



Requirements of the cavity supporting system

- Provide support of components: cavities, helium vessels, tuners, etc.
- Guarantee cavity (beam axis) alignment during entire life cycle
- Minimize thermal load

# Cavities positioning tolerance with respect to beam axis:

BUDGET OF TOLERANCE						
Step	Sub-step	Tolerances (3σ)	Total envelopes	recision		
Cryo-module assembly	Cavity and He vessel assembly	± 0.1 mm (TBD)	Positioning of the	- ion p		
	Supporting system assembly	± 0.2 mm (TBD)	cavity w.r.t. beam axis	truct		
	Vacuum vessel construction	± 0.2 mm (TBD)	± 0.5 mm	Cons		
Transport and handling (± 0.5 g any direction)	N.A.	± 0.1 mm (TBD)		ţ		
Testing/operation	Vacuum pumping		Stability of the cavity	tabili		
	Cool-down		w.r.t. beam axis	erm s		
	RF tests	± 0.2 mm (TBD)	± 0.5 mm	ong-te		
	Warm-up			Ľ		
	Thermal cycles					



Power coupler as support concept



- The power coupler double tube acts as vertical support and longitudinal positioner
- The design is simplified
  - Better thermal performance less heat conduction paths from room temperature

### Power coupler as support concept



#### Approximate weights and dimensions:

Weights (kg)					
Dressed cavity	200				
Short vacuum vessel	7000				
Long vacuum vessel	10000				
Lengths (mm)					
Double tube	300				
Cavities pitch (distance between consecutive double walled tubes)	1500				
Short vacuum vessel	7000 - 8000				
Long vacuum vessel	12000 – 13000				
Diameters (mm)					
Helium vessel	400				
Vacuum vessel	800-900				



Power coupler as support concept





### Inter-cavity support

- Sustain any load case (static, transport, thermal transient...)
- Allow alignment
- Keep alignment in steady state (warm and cold)
- Minimize stresses in helium tank
- Designed to work at 2K

Deformable

"triangle"

Allow contraction of helium tank

Designed by A.Vande Craen and J.B.Deschamps in collaboration with EN/MME



Design of spherical joint is being finished - to be tested soon



### Vacuum vessel / double tube interface

#### Designed by CNRS/IPNO



Courtesy of P.Duthil / S.Rousselot (CNRS/IPNO)



### **Introduction**

Design and tests by A.Vande Craen

• The UHV-CF flanges connection between the double tube of the power coupler and the helium vessel / cavity assembly is critical – a leak would contaminate beam vacuum

• In this mock-up, a bending moment is applied to this connection and the leak tightness is measured - these tests are carried out at room temperature

• One of the goals of this mock-up is the validation of the value of torque which is to be applied to the bolted connection





### Test setup and procedure

- A controlled torque is applied to each bolt to close the flanges
- A simple tube with the same stiffness and length of the double tube is used
- Copper gaskets from different manufacturers (*Garlock* and *Meca Design*) are used these gaskets were annealed at CERN
- A plastic cover is wrapped around the flanges and the space is filled with helium for the leak tightness measurements
- Two displacement sensors (LVDTs) are installed on each flange to measure possible opening
- The force is applied by a traction rod and measured by a load cell
- The load is applied until a leak is detected and then released. This process is carried out at least three times for a torque of 15 Nm and three times for a torque of 20 Nm (optimum value according to tests and value recommended by manufacturers)





Test setup and procedure



The tests were carried out with the help of the Mechanical Measurements Laboratory (EN/MME)



### **Results and conclusions**

- All leaks were detected for bending moments which are well beyond expected load cases
- The influence of the torque applied to the bolts is rather small

# Calculated bending moments for different cavity support scenarios:

	Inter-cavity support	M (kNm)			
	On both sides	0.09			
ſ	No inter-cavity support	2.12			
	On power coupler side only	1.82			
	On tuner side only	0.15			
	Loads are weight of components and transport acceleration (0.5 g in all directions)				

Test results - bending moment for leak:



These support scenarios are not realistic, since the absence of inter-cavity support on the tuner side of the dressed cavity assembly represents failure - the mechanical integrity of the double tube and the helium vessel would be compromised



### **Results and conclusions**

- The results change significantly from gasket to gasket
- A permanent leak was detected for gasket no. 5 after the first loading

• At no point during the tests was a separation of the flanges detected by the displacement sensors – stress relaxation of the gasket seems to be the cause of the leaks

#### **Possible explanations:**

- The mounting of the copper gaskets, a delicate operation, was not carried out by an experience person reproducibility becomes hard to achieve
- Gaskets from different manufacturers were used

#### Future work:

- The surface of the gaskets will be analysed
- Further tests will be carried out, involving the CERN vacuum group in the definition of an appropriate mounting procedure



### Test results - bending moment for leak:



**Introduction** 



- Validate the supporting and alignment concept
- Test critical components of unknown behaviour, the interface with vacuum vessel and the inter-cavity support, during assembly and cool-down
- Validate thermal calculations namely the thermal model of actively cooled double tube
- First tests foreseen for the summer of 2012



### Design – in progress

• Double tube, inter-cavity support and interface with vacuum vessel are the "real" components of this mock-up.

• A simplified cold mass is designed so that its mechanical stiffness is similar to the real cavity/helium vessel assembly

- Weights are added to the cold mass to guarantee that the loads applied to the supporting components are identical to the "real" loads
- A welded/brazed pipe to be filled with LN2 is used to thermalize flanges of fake "cavities"
- MLI will be wrapped around cold mass

• Targets and windows on the vacuum vessel are used for alignment measurement (laser tracker and BCAM); wire positioning monitors may be added in a 2<sup>nd</sup> stage





### Design – in progress

#### Calculation of the stiffness of the mock-up "cavity"

The mock-up cavity torsion and bending stiffness should be as close as possible to the ones of the real dressed cavity



#### Calculation of the weights to be added to the mock-up cold mass

For the mock-up cavity, force and moment at the interface with the vacuum vessel should match those of the real dressed cavity assembly (including tuner)







- The "cavities" are filled with liquid nitrogen and the flanges to which the inter-cavity supports are attached are thermalized
- The double tubes are cooled by a flow of gaseous nitrogen between 77 and 300 K heaters guarantee 300 K at the vacuum vessel / double tube interface.
- The cold mass alignment will be measured for different combinations of cold / warm "cavities" and double tubes



### Cryogenic scheme

Calculations by R.Bonomi – see presentation SPL Thermal studies (04/05)

- This mock-up will allow the validation of the thermal model of the actively cooled double tube critical aspect of the SPL Short Cryo-module design
- The temperature profile of the double tube walls and the required heating power at the vacuum vessel interface were calculated for different GN<sub>2</sub> mass flows

Mass flow (req vap power)	100 mg/s (20 W)		200 mg/s (40 W)		300 mg/s (60 W)	
P <sub>rf</sub>	ON	OFF	ON	OFF	ON	OFF
Q <sub>bath</sub> [W]	<b>9.145</b> ±5 mW	<b>3.962</b> ±0.5 mW	<b>4.735</b> ±5 mW	<b>1.834</b> ±1 mW	<b>3.476</b> ±4 mW	<b>1.392</b> ±1 mW
Q <sub>heater</sub> [W]	9.681	22.698	24.508	35.830	36.872	46.172
ΔL [mm]	0.408	0.552	0.543	0.640	0.617	0.685
ΔL tot [mm]	0.144		0.097		0.068	

#### **Results for different mass flows:**



#### Temperature profile for 300 mg/s:



### Instrumentation scheme



• Alignment – two lines of four targets (one per flange) should provide a comprehensive view of the cold mass movements

• The alignment measurements will be complemented by strain measurements on the double tubes external walls and displacement sensors between the two cavities

• **Thermometers** – Various Pt100 sensors will be placed on the cold mass, under vacuum. The temperature measurements on the double tubes walls and inter-cavity supports are fundamental for understanding the functioning of the mock-up components



### Some components





# Thank you for your attention

# Spare slides



"Standard" supporting scheme



Two-support preferable (isostatic - well defined forces on supports) If cavity straightness not enough...





"Standard" supporting scheme with third support





## Additional cavity support



Need for support : cavities alignment, structural integrity

Why an inter-cavity support: double tube can take full compressive load, heat load, assembly simplicity, thermal transients