CONCEPTUAL DRAFT FOR A HE-II BASED ULTRA COLD NEUTRON SOURCE IN THE MODERATOR COOLING BLOCK

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- How to create ultra cold neutrons (UCN)
- MCNP Simulation results for an ESS UCN source
- Experimental investigation of He-II
- Conclusion of results & outlook



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OVERVIEW

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Suitable materials for an UCN source

- In general the absorption cross-section increases with lower neutron energies
- Low capture cross-section more important for UCN gain then high elastic scattering cross-section
- \rightarrow Just a few materials are suitable for UCN applications

Isotope	
² H (Deuterium)	 Low absorption cross section but high elastic scattering cross section Solid at ultra cold temperatures Extended safety measures needed (high flammable gas)
⁴ He	 ✓ In phase II condensed (He-II) super thermal moderation properties ✓ No neutron capturing ✓ Inert × He-II is super fluid → Elaborate sealing needed × ³He contaminants can significantly reduce the UCN gain
¹² C	✓ No isotope separation needed (>98% abundance)
¹⁵ N	× Natural abundance to low \rightarrow Isotope separated highly expensive
¹⁶ O	✓ No isotope separation needed (>99% abundance)
²⁰⁸ Pb	Isotopic pure highly expensive (>1650\$/g)

¹H has a high capture cross-section!

→ Contaminations in a material are decreasing the UCN gain massively



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Suitable materials for an UCN source – superfluid He-II

- Phase transistion from liquid ⁴He in superfluid phase (He-II) at **2,17K**
- Plainly simple temperature reduction of L⁴He bath by pressure reduction:





Superthermal process:

- High energy transfer for ~8,9 Å neutrons to He-II (in just one interaction directly to UCN)
 → Premoderation should be optimised for high 8,9 Å gain
- Energy transfer to a "thermal reservoir" in He-II (system not in thermal equilibrium)
 → Effective UCN temperature can be lower then He-II temperature
- Upscattering Process is suppresed
- He-II has the highest known thermal conductivity
 → Heat is directly transferred to surrounding surface

He-II is a good choice for an UCN converter



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#2



Free

ω

Phonons

Neutrons

Rotons

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[1] C. Haberstroh – Flüssigheliumversorgung, TUDPress, 2010

[2] J. Yoder - Measurement of wall relaxation times of polarised ³He in bulk: Liquid ⁴He for the neutron electric dipole moment experiment. Diss. University of Ilinois, 2010



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Concept 1:

• UCN converter based on

3 stage coaxial design

- Converter medium: ⁴He-II
- Location: Moderator-Cooling-Block (MCB)

2 origin design:

- 1. Moderation of fast neutrons in thermal and cold moderator shell
- Neutron guide optimised f
 ür 8,9Å neutrons from VCN moderator to He-II converter
 - Guiding of UCN:
 - Option 1: Vertical
 - > Option 2: Horizontal through beamport



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Advantages of MCB location:

- Close to spallation center → high neutron flux but also high heat load
- Supply with different coolants (H₂O, LD₂) already close to location
- Shielding blocks can be replaced by UCN source
- LD_2 moderator close \rightarrow cold neutrons can be extracted for conversion





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MCNP simulation model – Calculation of UCN production rate

- UCN production rate P_{UCN} [cm⁻³ s⁻¹] figure of merit of UCN source
 - \rightarrow UCNs can not be transported directly with MCNP:

$$P_{\rm UCN}(V_{\rm c}) = N \,\sigma V_{\rm c} \frac{k_{\rm c}}{3\pi} \int_0^\infty \frac{{\rm d}\phi}{{\rm d}\lambda} s(\lambda) \lambda \,{\rm d}\lambda$$
^[4]

With

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 V_C : UCN potential N: Number of density of ⁴He atoms K_C : Cut of wavenumber for UCNs σ: Bound atom cross section of ⁴He



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[4] Schmidt-Wellenburg et al. - Ultra cold neutron production by multiphonon processes in superfluid helium under pressure – Nuclear Instruments and Methods in Physics Research A, 2009

MCNP simulation model: Concept 1



Baseline geometry: Al 6061-T6 vessel 3mm wall size filled with He-II @ 1K $V_{He-II} = 24233 \text{ cm}^3$ $\rightarrow P_{UCN} = 2.16E+03 \text{ cm}^{-3} \text{ s}^{-1}$ Gain in UCN production < 2% Modified shell concept under further investigation Thermal moderator thickness a [cm]



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MCNP simulation model: Concept 2

Concept 2: "Plain & simple"

- \rightarrow Aluminium vessel with minimized wall thickness
- → Maximized He-II volume
- → Passive He-II heatpipe design designated to remove heatload from UCN source

Additional factors for high performance:

- → Purification of ⁴He-II (reduction of contaminants ³He, $H_{2.}$)
- \rightarrow Coating of inner walls:
 - High Pseudo-Fermi potential of coating material compared to UCN energy needed \rightarrow ⁵⁸Ni





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Experimental investigations of He-II planned at Forschungszentrum Jülich

256 W

71 W

328 W



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- Glass-cryostate for visual investigation of the ⁴He-I to ⁴He-II phase-change
- Filling of glass vessel by connection to Helium dewar
- Cooling of ⁴He bath from 4,2K to 1,6K by pressure reduction with vacuum pump to induce phase-change
- Investigating phase stability by applying heat load into the center of the bath





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Bath temperature:	4,2 K
Pressure:	1000 mbar
Bath filling	100 %



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Bath temperature:	1,6 K	
Pressure:	7,6 mbar	Phase II
Bath filling	58 %	



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#12

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absorber

Taserbeen Resinner

Laser for apply of heat load into the He-II volume:

1,5W @ 445nm

- Low absorption in the glas vessel \rightarrow heat deposition into the absorber in the center of the He-II bath
- Focus optics allows beam broadening to ~10x3mm on absorber → Power density max. ~ 50mW/mm²
- Focused (~0,2x0,01mm) \rightarrow power density max. ~160W/mm²

Power control in two ways:

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- \rightarrow Continious wave power reduction with gray filters
- \rightarrow Pulse width modulation to reduce average power of beam
- \rightarrow Simulation of pulse structure of ESS proton beam possible



Flexible setup to taylor the laser beam in regard to the expected heat loads (MCNP) for an experimental simulation of the ESS conditions



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Second version of glass vessel:

- \rightarrow Investigation of mixing behaviour He-I <-> He-II
- → Investigation of limits for heat transport through limited cross section area







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Results

• 3 stage coaxial UCN source design based on He-II as conversion medium has been evaluated in MCNP

 \rightarrow Coaxial shell design is not effient to increase the UCN production rate

- → Best option is a "plain and simple" design:
 - \rightarrow Aluminium vessel with minimized wall thickness
 - → Maximized He-II volume
 - \rightarrow Passive He-II heatpipe design to remove heatload from UCN source

Outlook

- Experimental investigations on He-II regarding:
 - Phase stability
 - Heat conductivity
 - → Experimental simulation of ESS conditions based on MCNP simulation results (expected heatload, pulse structure):
 - Heatload deposition in the center of He-II volume
 - Heatload deposition in the vessel walls
 - Limits for crossection area for heat transport through He-II



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Thank you for your attention!